Community Solar Project Interconnection
Community Solar Project System Impact Study Report

Completed for
("Applicant")
OCS107

Proposed Point of Interconnection
Circuit 5P15 Kennedy Substation

June 10, 2025

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1.0 DESCRIPTION OF THE COMMUNITY SOLAR PROJECT

("Applicant") proposed interconnecting 2.25 MW of new generation to PacifiCorp's ("Public Utility") circuit 5P15 out of Kennedy substation located in Multnomah County, Oregon. The ("Project") will consist of nine (9) CPS SCH275KTL-DO/US-800, 275kVA, string inverters, for a total requested output of 2.25 MW. The requested commercial operation date is January 26, 2027.

The Public Utility has assigned the Project "OCS107."

2.0 APPROVAL CRITERIA FOR TIER 4 INTERCONNECTION REVIEW

Pursuant to the Section I(1) of the Public Utility's CSP Interconnection Procedures, a Public Utility must use the Tier 4 review procedures for an application to interconnect a Community Solar Project that meets the following requirements:

(a) The Community Solar Project does not qualify for or failed to meet Tier 2 review requirements; and
(b) The Community Solar Project must have a nameplate capacity of three (3) megawatts or less.

3.0 SCOPE OF THE STUDY

Pursuant to Section I(6)(g) of the CPS Interconnection Procedures, the System Impact Study Report shall consist of: (1) the underlying assumptions of the study; (2) a short circuit analysis; (2) a stability analysis; (3) a power flow analysis; (4) voltage drop and flicker studies; (5) protection and set point coordination studies; (6) grounding reviews; (7) the results of the analyses; and (8) any potential impediments to providing the requested Interconnection Service, including a non-binding informational NRIS portion that addresses the additions, modifications, and upgrades to the Public Utility's Transmission System that would be required at or beyond the point at which the Interconnection Facilities connect to the Public Utility's Transmission System to accommodate the interconnection of the CSP Project In addition, the System Impact Study shall provide a list of facilities that are required as a result of the Community Solar Project request and non-binding good faith estimates of cost responsibility and time to construct.

The information contained in this study report is based on preliminary information and not to be used for construction.

4.0 PROPOSED POINT OF INTERCONNECTION

The Applicant's proposed Community Solar Project is to be interconnected to the Public Utility's distribution circuit 5P15 out of Kennedy substation. The proposed Point of Interconnection will be located at approximately 45.598534, -122.633542 located in Multnomah County, Oregon. Figure 1 below is a one line diagram that illustrates the interconnection of the proposed generating facility to the Public Utility's system.

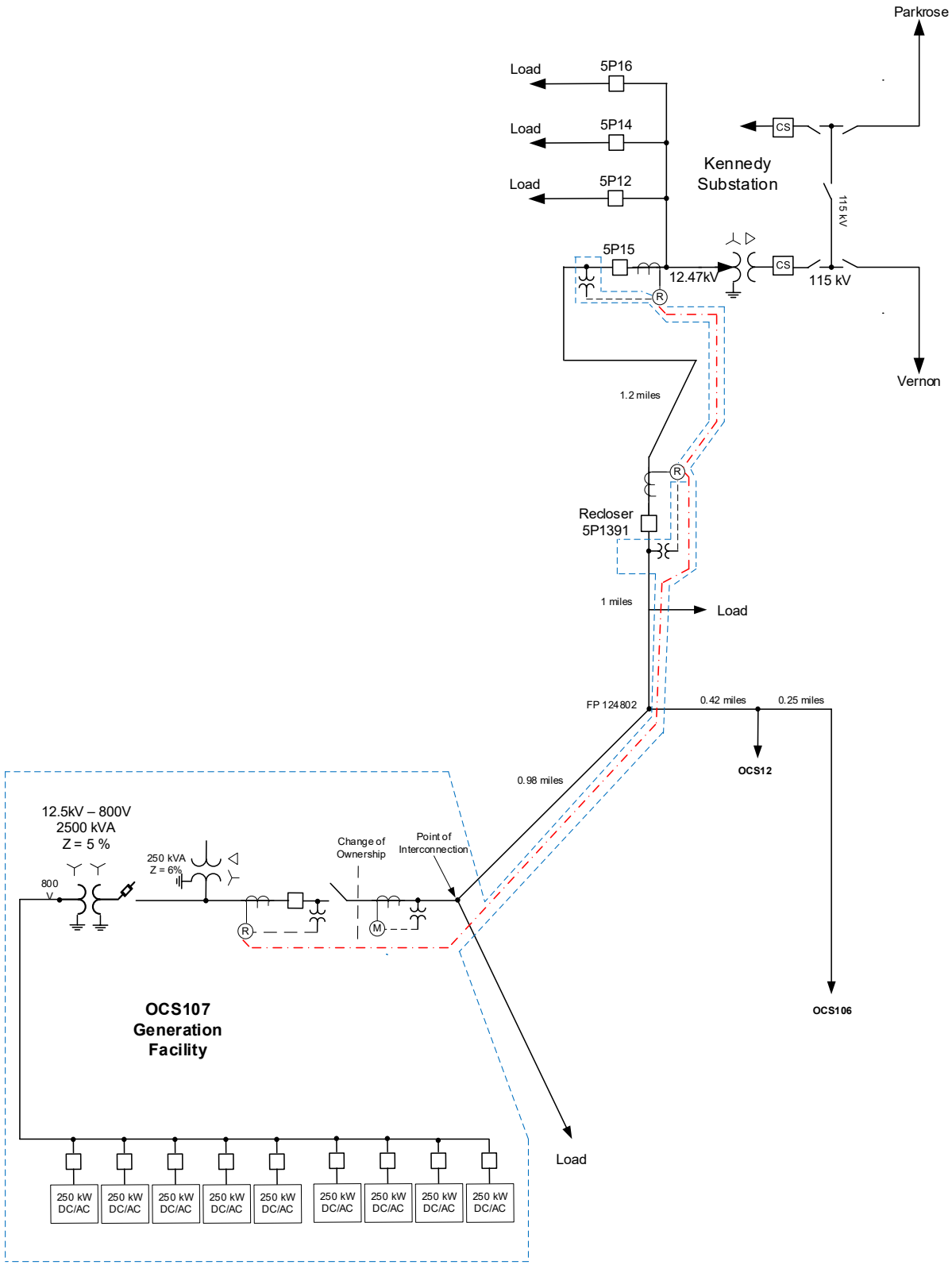


Figure 1: System One Line Diagram

5.0 STUDY ASSUMPTIONS

- All active higher-priority requests for transmission service and/or generator interconnection service (including requests in the traditional interconnection queue and other requests in the Community Solar queue) in the local area of the requested POI will be considered in this study and are listed in Appendix 1. If any of these requests are withdrawn, the Public Utility reserves the right to restudy this request, as the results and conclusions contained within this study could significantly change.
- The Applicant's request for interconnection service in and of itself does not convey transmission service.
- This study assumes the Project will be integrated into Public Utility's system at the agreed upon and/or proposed Point of Interconnection.
- The Applicant will construct and own any facilities required between the Point of Interconnection and the Project unless specifically identified by the Public Utility.
- Line reconductor or fiber underbuild required on existing poles will be assumed to follow the most direct path on the Public Utility's system. If during detailed design the path must be modified it may result in additional cost and timing delays for the Applicant's project.
- Generator tripping may be required for certain outages.
- All facilities will meet or exceed the minimum Western Electricity Coordinating Council ("WECC"), North American Electric Reliability Corporation ("NERC"), and Public Utility performance and design standards.
- There is a planned reconfiguration to move approximately 640kVA of load from 5P476 out of Columbia substation onto 5P15 by closing SW313 and opening SW360, this will be the new standard configuration on 5P15, this has been built into the CYME models. The MDL at the feeder for 5P15 before this reconfiguration is 3.58MW. CYME simulations after switching put the new MDL at 3.98MW, this value will be used in Sections 6.3 and 6.4.
- OCS012 and OCS106 are to be assumed completed and online prior to OCS107. Their loading must be accounted for in the MDL for this study.
- This report is based on information available at the time of the study. It is the Applicant's responsibility to check the Public Utility's web site regularly for transmission system updates (https://www.oasis.oati.com/ppw)

6.0 REQUIREMENTS

6.1 COMMUNITY SOLAR PROJECT REQUIREMENTS

The Community Solar Project and interconnection equipment owned by the Applicant are required to operate under constant power factor mode with a unity power factor setting unless specifically requested otherwise by the Public Utility. The Community Solar Project is expressly forbidden from actively participating in voltage regulation of the Public Utilities system without written request or authorization from the Public Utility. The Community Solar Project shall have sufficient reactive capacity to enable the delivery of 100 percent of the plant output to the POI at unity power factor measured at 1.0 per unit voltage under steady state conditions.

Generators shall be capable of operating under Voltage-reactive power mode, Active power-reactive power mode, and Constant reactive power mode as per IEEE Std. 1547-2018. This project shall be capable of activating each of these modes one at a time. The Public Utility reserves the right to specify any mode and settings within the limits of IEEE Std 1547-2018 needed before or after the Community Solar Project enters service. The Applicant shall be responsible for implementing settings modifications and mode selections as requested by the Public Utility within an acceptable timeframe. The reactive compensation must be designed such that the discreet switching of the reactive device (if required by the Applicant) does not cause step voltage changes greater than +/-3% on the Public Utility's system. In all cases the minimum power quality requirements in Public Utility's Engineering Handbook section 1C shall be met and are available at https://www.pacificpower.net/about/power-quality-standards.html. Requirements specified in the System Impact Study that exceed requirements in the Engineering Handbook section 1C power quality standards shall apply.

All generators must meet applicable WECC low voltage ride-through requirements as specified in the interconnection agreement.

The Applicant will be required to install a transformer that will hold the phase to neutral voltages within limits when the generation facility is isolated with the Transmission Provider's local system until the generation disconnects. The minimum recommended size of this grounding transformer is 250kVA with 6% impedance. The circuit that the project is connecting to is a 12.47kV four wire multi-grounded circuit with line to neutral connected load. Figure 1 shows the addition of a wye – delta grounding transformer of adequate power size and impedance that will meet the requirement.

6.2 Transmission System Modifications

Under the normal and contingency configurations, there are no identified power flow restrictions with OCS0107 generation online. No Transmission system modifications are required.

6.3 Distribution/Transmission Line Modifications

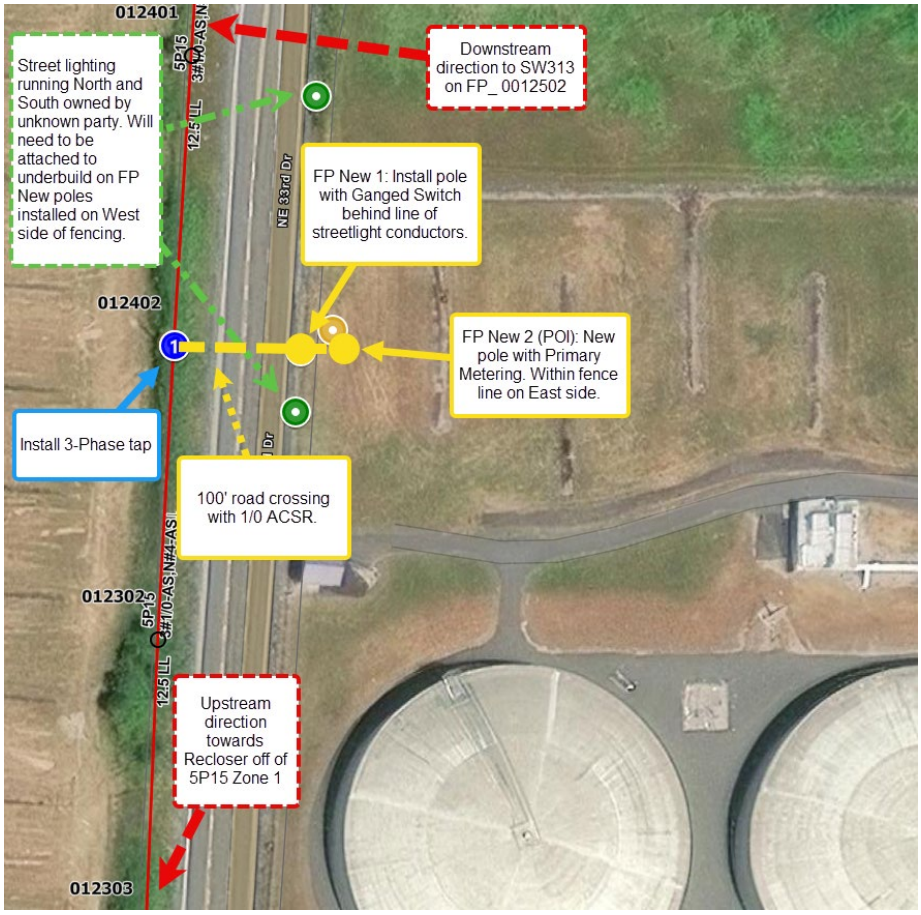
Distribution system feeder 5P15 minimum daytime load (MDL) is 1.7 MW. The Applicant's proposed generating facility is located 16,752 ft. from the Kennedy substation and 10,474 ft from upstream recloser. The site is downstream from a recloser facility point ("FP") 01101001.0134505 from the mainline with an MDL of 0.96 MW. The site downstream to the tap going to OCS012 and OCS106. The Kennedy 5P15 system is 12.47kV$_{L-L}$ operated in a grounded wye - grounded wye configuration. The added nameplate capacity from OCS107 overruns MDL at CB 5P15 by approximately 0.6MW or 115%, and MDL at the recloser 5P1391 by 1.3MW or 140%.

The Applicant's proposed Point of Interconnection (POI) is on the east side of 33rd NE Drive across from FP 01101001.0012402. The east side of the road has streetlights going north and south that do not belong to Public Utility. A new pole will be set to span the

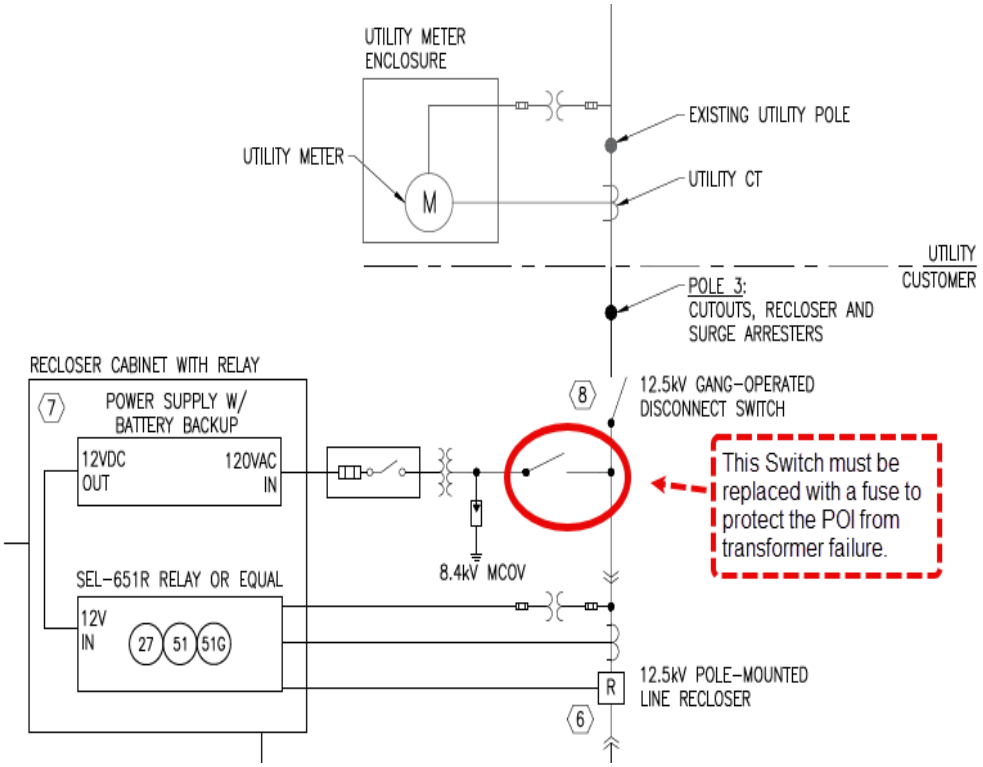
primary over the existing streetlight wiring. New utility poles install on east side may require FAA permits due to proximity to PDX airport.

The following distribution system modifications will be required to provide a POI at the Applicant's requested location:

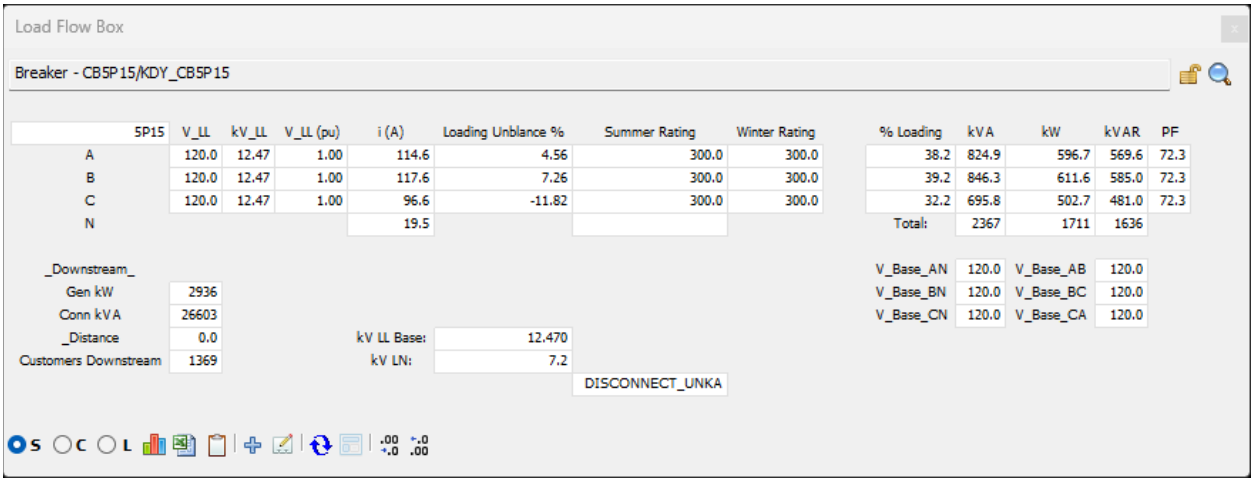
- **FP_0122902 to FP New 1:** Install 3-phase tap armatures to pole, run 100ft of new 3-phase 1/0 ACSR for road crossing to new pole on east side of the road in-between existing non-Public Utility streetlight poles to the north and south. Installed ganged Switch at POI pole. Existing streetlight wires will need to be attached to our new pole to prevent slapping from wind if they are installed on the west side of the fencing instead of the Applicant's lot.
- **FP New 1 to FP New 2 (POI):** Install new pole within Applicant's lot for Primary Metering.



- The Applicant must add fusing between their recloser cabinet's PT and the source side of the line recloser.


UTILITY METER ENCLOSURE
UTILITY METER
M
EXISTING UTILITY POLE
UTILITY CT
UTILITY
CUSTOMER
POLE 3:
CUTOUTS, RECLOSER AND SURGE ARRESTERS
RECLOSER CABINET WITH RELAY
7
POWER SUPPLY W/ BATTERY BACKUP
12VDC OUT
120VAC IN
SEL-651R RELAY OR EQUAL
12V IN
27
51
51G
8
12.5kV GANG-OPERATED DISCONNECT SWITCH
This Switch must be replaced with a fuse to protect the POI from transformer failure.
8.4kV MCOV
R
12.5kV POLE-MOUNTED LINE RECLOSER
6

After OCS12 and OCS106 are Online:

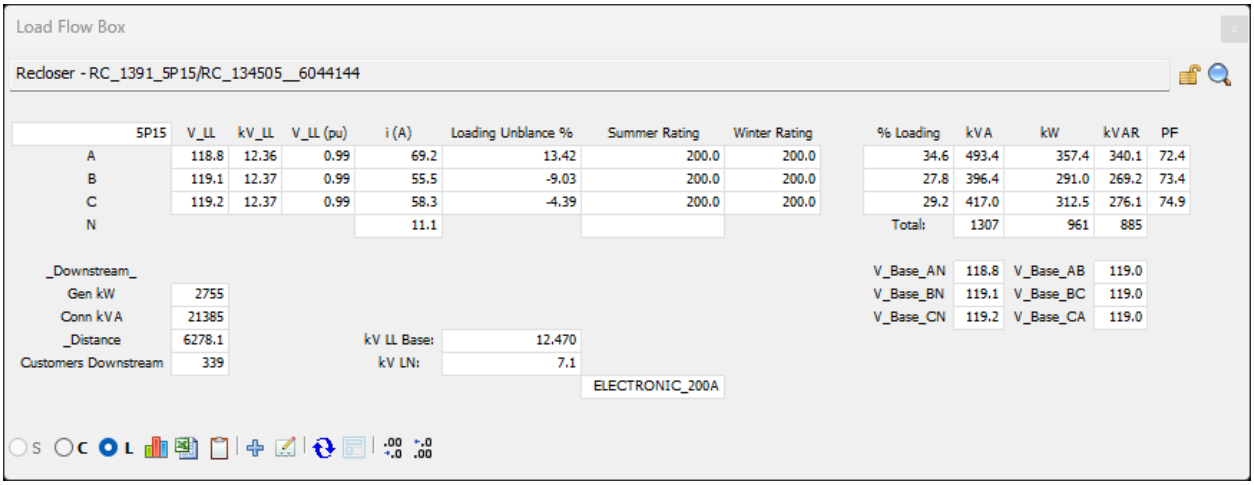


Load Flow Box

Breaker - CB5P15/KDY_CB5P15

5P15	V_LL	kV_LL	V_LL (pu)	i (A)	Loading Unblance %	Summer Rating	Winter Rating	% Loading	kVA	kW	kVAR	PF
A	120.0	12.47	1.00	114.6	4.56	300.0	300.0	38.2	824.9	596.7	569.6	72.3
B	120.0	12.47	1.00	117.6	7.26	300.0	300.0	39.2	846.3	611.6	585.0	72.3
C	120.0	12.47	1.00	96.6	-11.82	300.0	300.0	32.2	695.8	502.7	481.0	72.3
N				19.5				Total:	2367	1711	1636	

Downstream				V_Base_AN	120.0	V_Base_AB	120.0
Gen kW	2936			V_Base_BN	120.0	V_Base_BC	120.0
Conn kVA	26603			V_Base_CN	120.0	V_Base_CA	120.0
_Distance	0.0	kV LL Base:	12.470				
Customers Downstream	1369	kV LN:	7.2				
				DISCONNECT_UNKA			



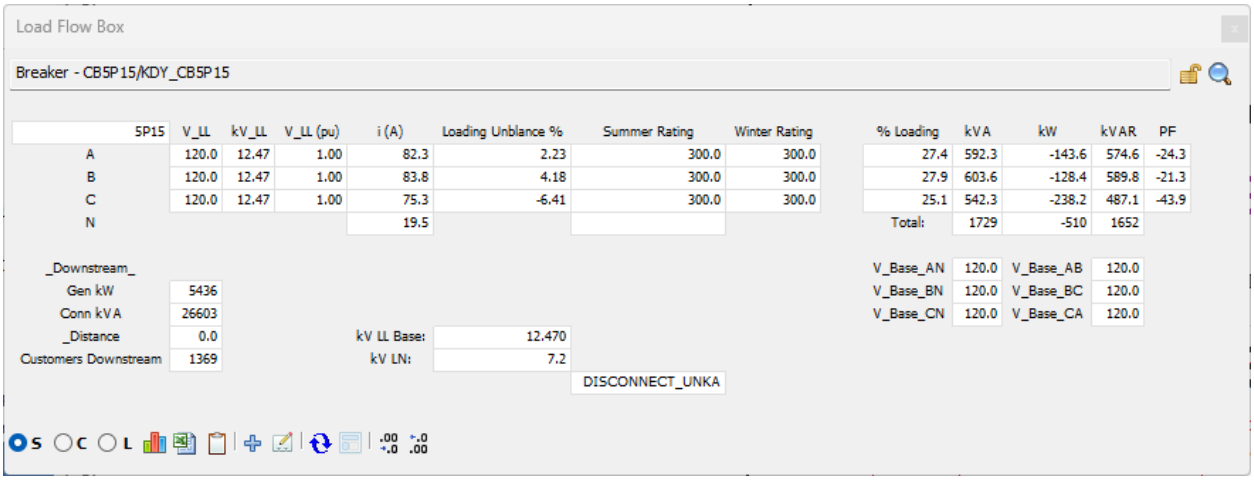
Load Flow Box

Recloser - RC_1391_5P15/RC_134505__6044144

5P15	V_LL	kV_LL	V_LL (pu)	i (A)	Loading Unblance %	Summer Rating	Winter Rating	% Loading	kVA	kW	kVAR	PF
A	118.8	12.36	0.99	69.2	13.42	200.0	200.0	34.6	493.4	357.4	340.1	72.4
B	119.1	12.37	0.99	55.5	-9.03	200.0	200.0	27.8	396.4	291.0	269.2	73.4
C	119.2	12.37	0.99	58.3	-4.39	200.0	200.0	29.2	417.0	312.5	276.1	74.9
N				11.1				Total:	1307	961	885	

Downstream				V_Base_AN	118.8	V_Base_AB	119.0
Gen kW	2755			V_Base_BN	119.1	V_Base_BC	119.0
Conn kVA	21385			V_Base_CN	119.2	V_Base_CA	119.0
_Distance	6278.1	kV LL Base:	12.470				
Customers Downstream	339	kV LN:	7.1				
				ELECTRONIC_200A			

After OCS107 Online:

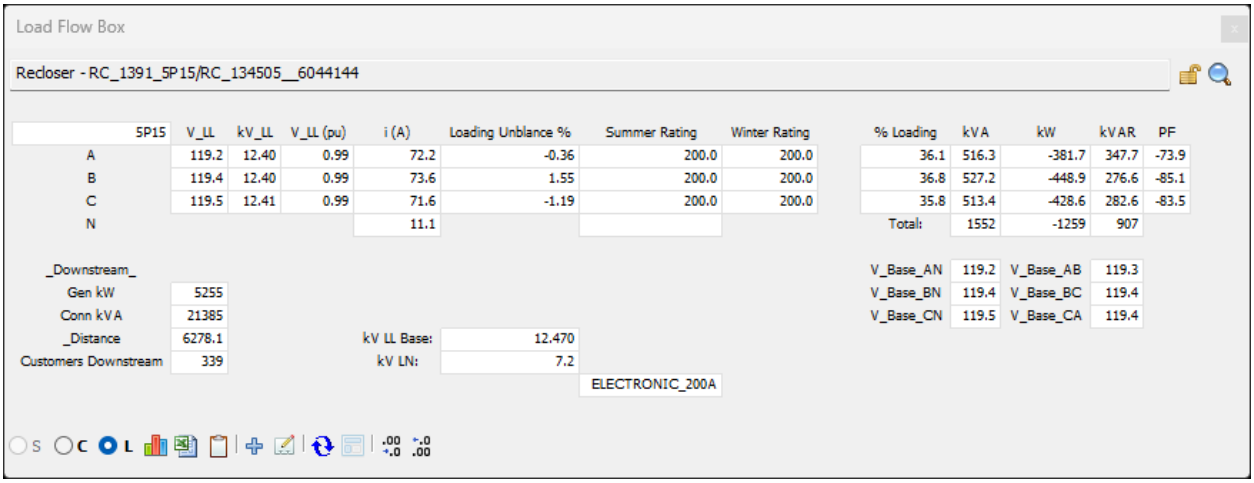


Load Flow Box

Breaker - CB5P15/KDY_CB5P15

5P15	V_LL	kV_LL	V_LL (pu)	i (A)	Loading Unblance %	Summer Rating	Winter Rating	% Loading	kVA	kW	kVAR	PF
A	120.0	12.47	1.00	82.3	2.23	300.0	300.0	27.4	592.3	-143.6	574.6	-24.3
B	120.0	12.47	1.00	83.8	4.18	300.0	300.0	27.9	603.6	-128.4	589.8	-21.3
C	120.0	12.47	1.00	75.3	-6.41	300.0	300.0	25.1	542.3	-238.2	487.1	-43.9
N				19.5				Total:	1729	-510	1652	

Downstream				V_Base_AN	120.0	V_Base_AB	120.0
Gen kW	5436			V_Base_BN	120.0	V_Base_BC	120.0
Conn kVA	26603			V_Base_CN	120.0	V_Base_CA	120.0
_Distance	0.0	kV LL Base:	12.470				
Customers Downstream	1369	kV LN:	7.2				
				DISCONNECT_UNKA			



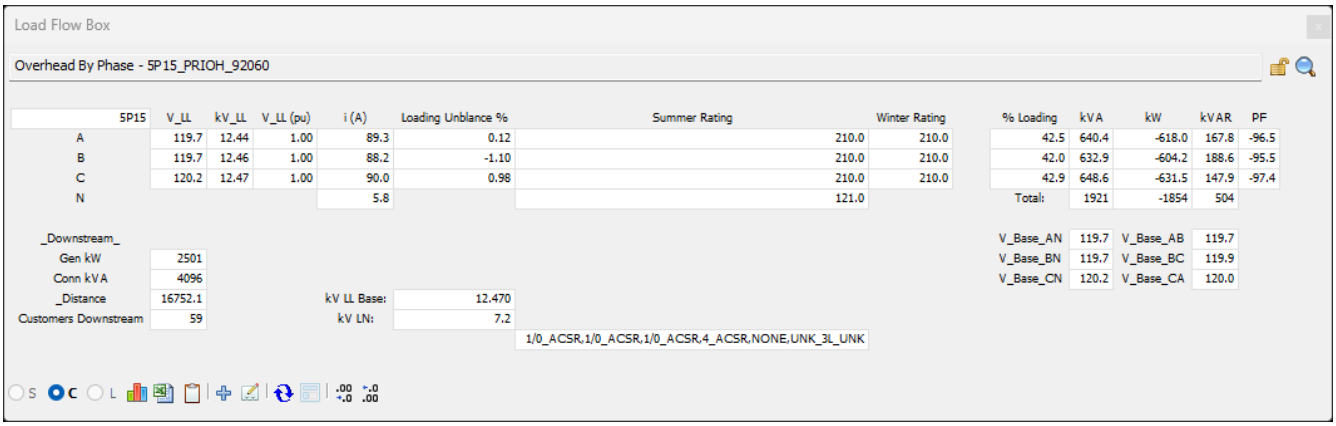
Load Flow Box

Recloser - RC_1391_5P15/RC_134505__6044144

5P15	V_LL	kV_LL	V_LL (pu)	i (A)	Loading Unblance %	Summer Rating	Winter Rating	% Loading	kVA	kW	kVAR	PF
A	119.2	12.40	0.99	72.2	-0.36	200.0	200.0	36.1	516.3	-381.7	347.7	-73.9
B	119.4	12.40	0.99	73.6	1.55	200.0	200.0	36.8	527.2	-448.9	276.6	-85.1
C	119.5	12.41	0.99	71.6	-1.19	200.0	200.0	35.8	513.4	-428.6	282.6	-83.5
N				11.1				Total:	1552	-1259	907	

Downstream				V_Base_AN	119.2	V_Base_AB	119.3
Gen kW	5255			V_Base_BN	119.4	V_Base_BC	119.4
Conn kVA	21385			V_Base_CN	119.5	V_Base_CA	119.4
_Distance	6278.1	kV LL Base:	12.470				
Customers Downstream	339	kV LN:	7.2				
				ELECTRONIC_200A			

No Voltage drop or Over Current loading for the 1/0 ACSR lines at FP 01101001.0012402 for OCS107:



Load Flow Box

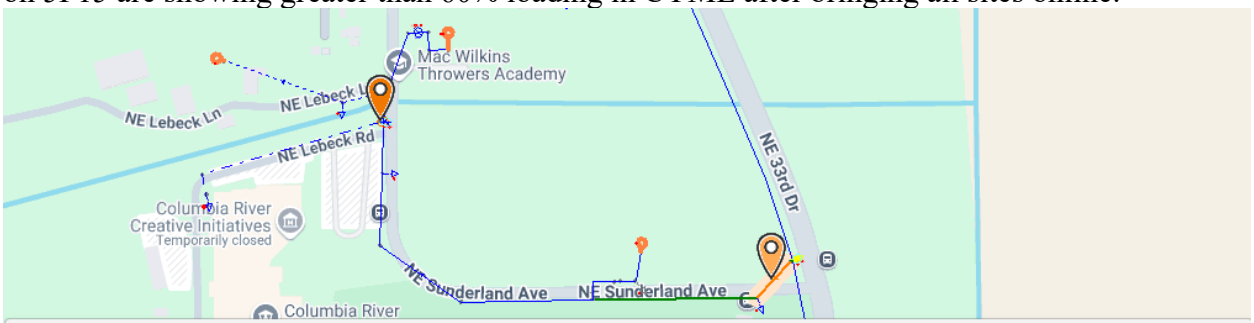
Overhead By Phase - 5P15_PRIOH_92060

5P15	V_LL	kV_LL	V_LL (pu)	i (A)	Loading Unblance %	Summer Rating	Winter Rating	% Loading	kVA	kW	kVAR	PF
A	119.7	12.44	1.00	89.3	0.12	210.0	210.0	42.5	640.4	-618.0	167.8	-96.5
B	119.7	12.46	1.00	88.2	-1.10	210.0	210.0	42.0	632.9	-604.2	188.6	-95.5
C	120.2	12.47	1.00	90.0	0.98	210.0	210.0	42.9	648.6	-631.5	147.9	-97.4
N				5.8		121.0		Total:	1921	-1854	504	

Downstream					
Gen kW	2501			V_Base_AN	119.7	V_Base_AB	119.7
Conn kVA	4096			V_Base_BN	119.7	V_Base_BC	119.9
_Distance	16752.1	kV LL Base:	12.470	V_Base_CN	120.2	V_Base_CA	120.0
Customers Downstream	59	kV LN:	7.2				

1/0_ACSR,1/0_ACSR,1/0_ACSR,4_ACSR,NONE,UNK_3L_UNK

With OCS106 online about 60% loading on the span from the tap to OCS12. No other conductors on 5P15 are showing greater than 60% loading in CYME after bringing all sites online:



Load Flow Box

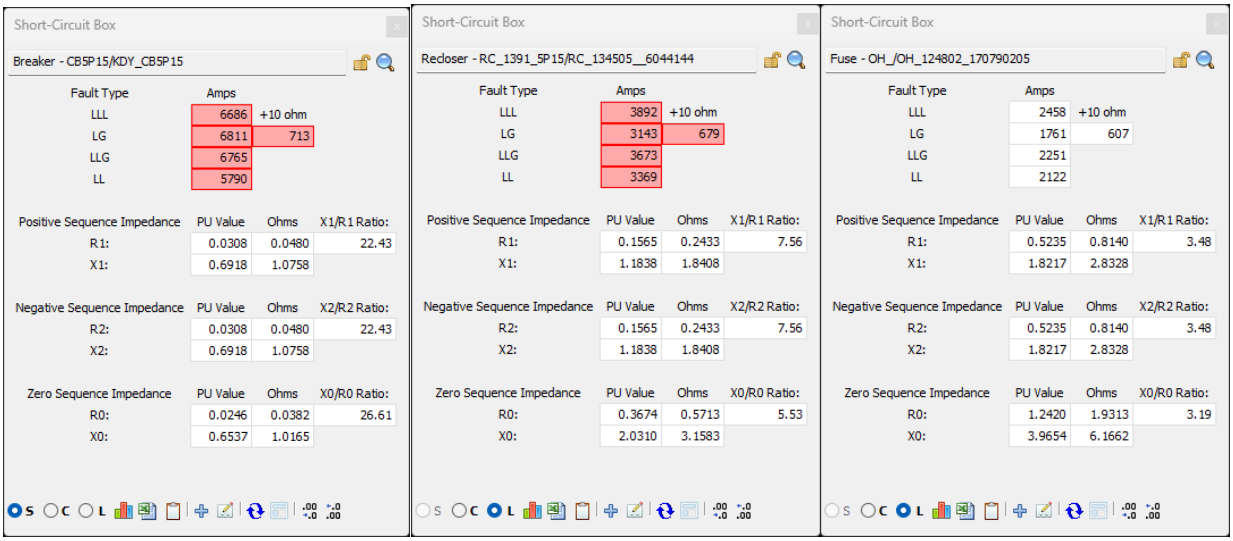
Overhead By Phase - 5P15_PRIOH_466943

5P15	V_LL	kV_LL	V_LL (pu)	i (A)	Loading Unblance %	Summer Rating	Winter Rating	% Loading	kVA	kW	kVAR	PF
A	119.6	12.43	1.00	97.1	-0.50	160.0	160.0	60.7	696.5	-695.2	42.0	-99.8
B	119.7	12.44	1.00	97.5	-0.14	244.0	244.0	40.0	699.8	-698.6	40.2	-99.8
C	120.0	12.45	1.00	98.2	0.64	244.0	244.0	40.3	706.9	-705.5	45.2	-99.8
N				1.6		121.0		Total:	2103	-2099	127	

Downstream					
Gen kW	2510			V_Base_AN	119.6	V_Base_AB	119.6
Conn kVA	866			V_Base_BN	119.7	V_Base_BC	119.7
_Distance	13725.8	kV LL Base:	12.470	V_Base_CN	120.0	V_Base_CA	119.8
Customers Downstream	8	kV LN:	7.2				

2_ACSR,2_CU,2_CU,4_ACSR,NONE,UNK_3L_UNK

Short Circuit Boxes all after both OCS12 and OCS106 are online:



Short-Circuit Box

Breaker - CB5P15/KDY_CB5P15

Fault Type	Amps	+10 ohm
LLL	6686	
LG	6811	713
LLG	6765	
LL	5790	

Positive Sequence Impedance	PU Value	Ohms	X1/R1 Ratio:
R1:	0.0308	0.0480	22.43
X1:	0.6918	1.0758	

Negative Sequence Impedance	PU Value	Ohms	X2/R2 Ratio:
R2:	0.0308	0.0480	22.43
X2:	0.6918	1.0758	

Zero Sequence Impedance	PU Value	Ohms	X0/R0 Ratio:
R0:	0.0246	0.0382	26.61
X0:	0.6537	1.0165	

Short-Circuit Box

Recloser - RC_1391_5P15/RC_134505__6044144

Fault Type	Amps	+10 ohm
LLL	3892	
LG	3143	679
LLG	3673	
LL	3369	

Positive Sequence Impedance	PU Value	Ohms	X1/R1 Ratio:
R1:	0.1565	0.2433	7.56
X1:	1.1838	1.8408	

Negative Sequence Impedance	PU Value	Ohms	X2/R2 Ratio:
R2:	0.1565	0.2433	7.56
X2:	1.1838	1.8408	

Zero Sequence Impedance	PU Value	Ohms	X0/R0 Ratio:
R0:	0.3674	0.5713	5.53
X0:	2.0310	3.1583	

Short-Circuit Box

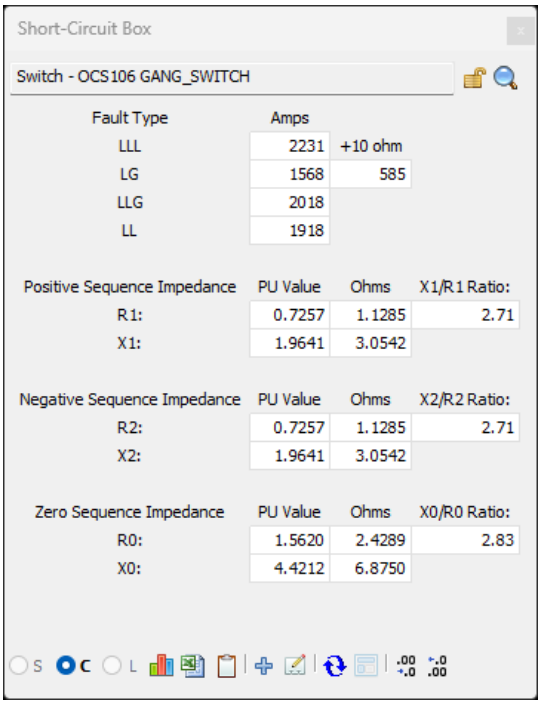
Fuse - OH_/OH_124802_170790205

Fault Type	Amps	+10 ohm
LLL	2458	
LG	1761	607
LLG	2251	
LL	2122	

Positive Sequence Impedance	PU Value	Ohms	X1/R1 Ratio:
R1:	0.5235	0.8140	3.48
X1:	1.8217	2.8328	

Negative Sequence Impedance	PU Value	Ohms	X2/R2 Ratio:
R2:	0.5235	0.8140	3.48
X2:	1.8217	2.8328	

Zero Sequence Impedance	PU Value	Ohms	X0/R0 Ratio:
R0:	1.2420	1.9313	3.19
X0:	3.9654	6.1662	



Short-Circuit Box

Switch - OCS106 GANG_SWITCH

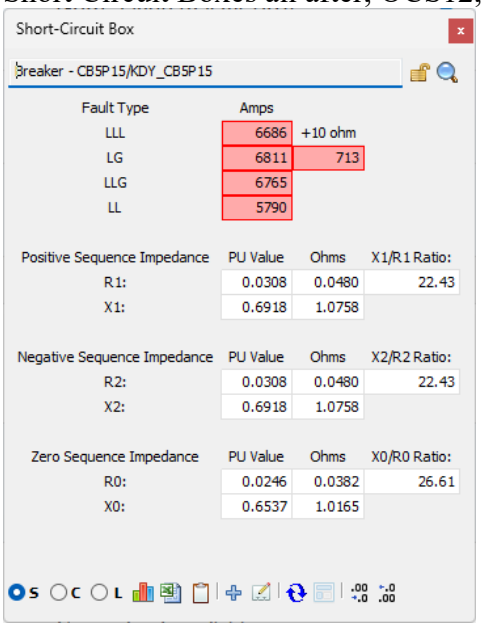
Fault Type	Amps	+10 ohm
LLL	2231	
LG	1568	585
LLG	2018	
LL	1918	

Positive Sequence Impedance	PU Value	Ohms	X1/R1 Ratio:
R1:	0.7257	1.1285	2.71
X1:	1.9641	3.0542	

Negative Sequence Impedance	PU Value	Ohms	X2/R2 Ratio:
R2:	0.7257	1.1285	2.71
X2:	1.9641	3.0542	

Zero Sequence Impedance	PU Value	Ohms	X0/R0 Ratio:
R0:	1.5620	2.4289	2.83
X0:	4.4212	6.8750	

Short Circuit Boxes all after, OCS12, OCS106, and OCS107 are online:


Short-Circuit Box

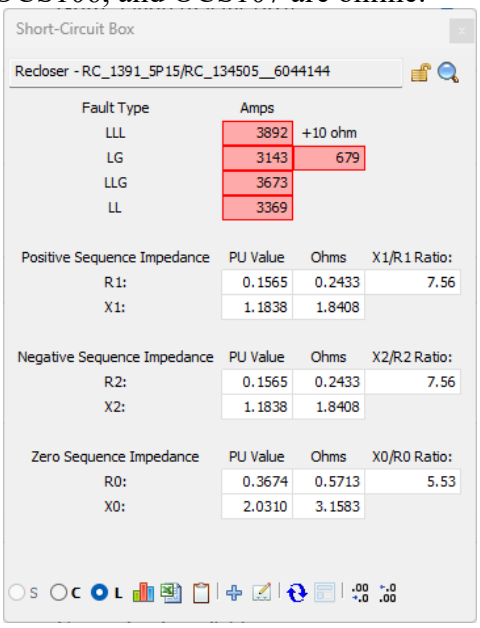
Breaker - CB5P15/KDY_CB5P15

Fault Type	Amps	+10 ohm
LLL	6686	
LG	6811	713
LLG	6765	
LL	5790	

Positive Sequence Impedance	PU Value	Ohms	X1/R1 Ratio:
R1:	0.0308	0.0480	22.43
X1:	0.6918	1.0758	

Negative Sequence Impedance	PU Value	Ohms	X2/R2 Ratio:
R2:	0.0308	0.0480	22.43
X2:	0.6918	1.0758	

Zero Sequence Impedance	PU Value	Ohms	X0/R0 Ratio:
R0:	0.0246	0.0382	26.61
X0:	0.6537	1.0165	


Short-Circuit Box

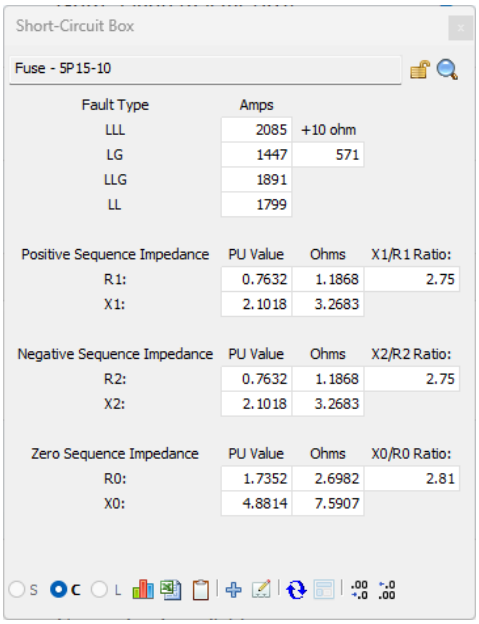
Recloser - RC_1391_5P15/RC_134505__6044144

Fault Type	Amps	+10 ohm
LLL	3892	
LG	3143	679
LLG	3673	
LL	3369	

Positive Sequence Impedance	PU Value	Ohms	X1/R1 Ratio:
R1:	0.1565	0.2433	7.56
X1:	1.1838	1.8408	

Negative Sequence Impedance	PU Value	Ohms	X2/R2 Ratio:
R2:	0.1565	0.2433	7.56
X2:	1.1838	1.8408	

Zero Sequence Impedance	PU Value	Ohms	X0/R0 Ratio:
R0:	0.3674	0.5713	5.53
X0:	2.0310	3.1583	


Short-Circuit Box

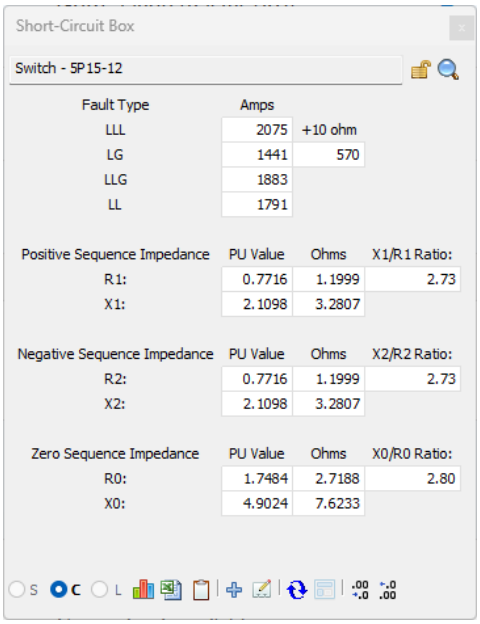
Fuse - 5P15-10

Fault Type	Amps	+10 ohm
LLL	2085	
LG	1447	571
LLG	1891	
LL	1799	

Positive Sequence Impedance	PU Value	Ohms	X1/R1 Ratio:
R1:	0.7632	1.1868	2.75
X1:	2.1018	3.2683	

Negative Sequence Impedance	PU Value	Ohms	X2/R2 Ratio:
R2:	0.7632	1.1868	2.75
X2:	2.1018	3.2683	

Zero Sequence Impedance	PU Value	Ohms	X0/R0 Ratio:
R0:	1.7352	2.6982	2.81
X0:	4.8814	7.5907	


Short-Circuit Box

Switch - 5P15-12

Fault Type	Amps	+10 ohm
LLL	2075	
LG	1441	570
LLG	1883	
LL	1791	

Positive Sequence Impedance	PU Value	Ohms	X1/R1 Ratio:
R1:	0.7716	1.1999	2.73
X1:	2.1098	3.2807	

Negative Sequence Impedance	PU Value	Ohms	X2/R2 Ratio:
R2:	0.7716	1.1999	2.73
X2:	2.1098	3.2807	

Zero Sequence Impedance	PU Value	Ohms	X0/R0 Ratio:
R0:	1.7484	2.7188	2.80
X0:	4.9024	7.6233	

6.4 EXISTING BREAKER MODIFICATIONS – SHORT-CIRCUIT

The increase in the fault duty on the system as the result of the addition of the generation facility with photovoltaic arrays fed through 9 – 275kVA CPS inverters connected to a 2.5 MVA 12.5 kV – 800 V transformer with 5 % impedance will not push the fault duty above the interrupting rating of any of the existing fault interrupting equipment.

6.5 PROTECTION REQUIREMENTS

The OCS107 Community Solar Project will need to disconnect from the network in a high-speed manner for faults on the 12.47 kV line on circuit 5P15 out of Kennedy substation. The minimum daytime load on circuit 5P15 is 1.7 MW which is below the maximum potential power output of the proposed OCS107 Community Solar Project facility plus existing generation on the circuit. Since the unbalance between the generation and load cannot be relied upon to cause the timely disconnection of the solar facility for faults on the 12.47 kV circuit beyond the circuit breaker a transfer trip circuit will be required between the circuit breaker and the OCS107 POI recloser at the solar facility. A deadline checking control circuit will be required for the circuit breaker to delay the automatic reclose if the generation at the solar facility is not disconnected due to a failure of the relay circuitry. This type of control requires installation of potential transformers on the line side of CB 5P15 to enable dead line check. Verify that directional overcurrent elements are enabled for the feeder.

The Community Solar Project is planned to be connected beyond an existing line recloser RC 5P1391 at facility point 01101001.0134505. During some daytime periods the load beyond the recloser can be as low as 0.96 MW which is less than the potential generation from the proposed Community Solar Project facility plus existing generations beyond the field recloser. Since the unbalance between the generation and load cannot be relied upon to cause the timely disconnection of the solar facility for faults on the 12.47 kV circuit beyond the recloser a transfer trip circuit will be required between the line recloser and the OCS107 POI recloser at the solar facility. A deadline checking control circuit will be required for the line recloser to delay the automatic reclose if the generation at the solar facility is not disconnected due to a failure of the relay circuitry. Voltage instrument transformers will need to be added to the load side of the line recloser for the deadline checking. Verify that directional overcurrent elements are enabled for the field recloser.

The 12.47 kV circuit recloser planned to be installed at the OCS107 project will need to be equipped with Schweitzer Engineering Laboratories (SEL) 651R relay/controller and voltage instrument transformers mounted on the utility side of the circuit recloser. The 651R will perform the following protection functions:

1. Detect faults on the 12.47 kV equipment at the solar-electric Community Solar Project
2. Detect faults on the 12.47 kV line to Kenndy substation
3. Monitor the voltage and react to under or over frequency, and/or magnitude of the voltage

4. Communicate with CB 5P15 to receive transfer trip from the circuit breaker for the opening of the feeder breaker or field recloser.

6.6 DATA REQUIREMENTS (RTU)

There are no SCADA requirements for this.

6.7 COMMUNICATION REQUIREMENTS

Install a 50' wood pole at the POI and a 60' wood pole in the Kennedy substation yard. Install an SEL-3031 radio link between the two locations. At the POI, connect the radio to the recloser's comm port. At Kennedy substation, connect the radio to the circuit breaker's relay.

6.8 SUBSTATION REQUIREMENTS

Kennedy substation

A voltage transformer will be installed on the line side of circuit breaker 5P15 to support the dead line check circuit. Conduit and control cable will be installed to support the voltage transformer installation. Conduit will be installed to support the fiber installation.

6.9 METERING REQUIREMENTS

Interchange Metering

The metering will be located on the high side of the Applicant generator step up transformer at the Point of Interconnection. The metering will be installed overhead on a pole per distribution DM construction standards. The Public Utility will procure, install, test, and own all revenue metering equipment. The metering will be bi-directional to measure KWH and KVARH quantities for both generation received, and back feed retail load delivered. There will be no additional station service metering for supplying generation load. The metering generation and billing data will be remotely interrogated via the Public Utility's MV90 data acquisition system.

Station Service/Construction Power

Prior to construction, Applicant must arrange construction power with the Public Utility as holding the certificated service territory rights for the area in which the load is physically located. Station service and temporary construction power metering shall conform to the Six State Electric Service Requirements manual.

Please note, prior to back feed, Applicant must arrange distribution voltage retail meter service for electricity consumed by the Project and arrange back up station service for power that will be drawn from the distribution line when the Project is not generating. Applicant must call the PCCC Solution Center 1-800-640-2212 to arrange this service. Approval for back feed is contingent upon obtaining station service.

7.0 COST ESTIMATE

The following estimate represents only scopes of work that will be performed by the Public Utility. Costs for any work being performed by the Applicant are not included.

Distribution System *Line extension and poles*	$70,000
Protection and Control *Engineering and relay settings review*	$70,000
Kennedy Substation *VT installation and SEL 651R*	$130,000
Metering *Metering package and engineering*	$13,000
Project Management *Project manager, project control specialist*	$18,000
Other *Capital surcharge, contingency, administrative support*	$66,000
Total	**$367,000**

*Any distribution line modifications identified in this report will require a field visit analysis in order to obtain a more thorough understanding of the specific requirements. The estimate provided above for this work could change substantially based on the results of this analysis. Until this field analysis is performed the Public Utility must develop the Project schedule using conservative assumptions. The Applicant may request that the Public Utility perform this field analysis, at the Applicant's expense, prior to the execution of an Interconnection Agreement in order to obtain more cost and schedule certainty.

Note: Costs for any excavation, duct installation and easements shall be borne by the Applicant and are not included in this estimate. This estimate is as accurate as possibly given the level of detailed study that has been completed to date and approximates the costs incurred by Public Utility to interconnect this Community Solar Project to Public Utility's electrical distribution or transmission system. An estimate, based on finer detail, will be calculated during the Facilities Study. The Applicant will be responsible for all actual costs, regardless of the estimated costs communicated to or approved by the Applicant.

8.0 SCHEDULE

The Public Utility estimates it will require approximately 18 months to design, procure and construct the facilities described in this report following the execution of an Interconnection Agreement. The schedule will be further developed and optimized during the Facilities Study.

Please note, the time required to perform the scope of work identified in this report appears to result in a timeframe that does support the Applicant's requested commercial operation date of January 26, 2027.

9.0 PARTICIPATION BY AFFECTED SYSTEMS

Public Utility has identified the following Affected Systems: None

10.0 APPENDICES

Appendix 1: Higher Priority Requests
Appendix 3: Property Requirements

10.1 APPENDIX 1: HIGHER PRIORITY REQUESTS

All active higher priority transmission service and/or generator interconnection and Community Solar Project requests will be considered in this study and are identified below. If any of these requests are withdrawn, the Public Utility reserves the right to restudy this request, as the results and conclusions contained within this study could significantly change.

Transmission/Generation Interconnection/Community Solar Queue Requests considered:

OCS012
OCS106

10.2 APPENDIX 3: PROPERTY REQUIREMENTS

Requirements for rights of way easements
Rights of way easements will be acquired by the Applicant in the Public Utility's name for the construction, reconstruction, operation, maintenance, repair, replacement, and removal of Public Utility's Interconnection Facilities that will be owned and operated by PacifiCorp. Applicant will acquire all necessary permits for the project and will obtain rights of way easements for the project on Public Utility's easement form.

Real Property Requirements for Point of Interconnection Substation
Real property for a point of interconnection substation will be acquired by an Applicant to accommodate the Applicant's project. The real property must be acceptable to Public Utility. Applicant will acquire fee ownership for interconnection substation unless Public Utility determines that other than fee ownership is acceptable; however, the form and instrument of such rights will be at Public Utility's sole discretion. Any land rights that Applicant is planning to retain as part of a fee property conveyance will be identified in advance to Public Utility and are subject to the Public Utility's approval.

The Applicant must obtain all permits required by all relevant jurisdictions for the planned use including but not limited to conditional use permits, Certificates of Public Convenience and Necessity, California Environmental Quality Act, as well as all construction permits for the project.

Applicant will not be reimbursed through network upgrades for more than the market value of the property.

As a minimum, real property must be environmentally, physically, and operationally acceptable to Public Utility. The real property shall be a permitted or able to be permitted use in all zoning districts. The Applicant shall provide Public Utility with a title report and shall transfer property without any material defects of title or other encumbrances that are not acceptable to Public Utility. Property lines shall be surveyed and show all encumbrances, encroachments, and roads.

Examples of potentially unacceptable environmental, physical, or operational conditions could include but are not limited to:

- Environmental: known contamination of site; evidence of environmental contamination by any dangerous, hazardous or toxic materials as defined by any governmental agency; violation of building, health, safety, environmental, fire, land use, zoning or other such regulation; violation of ordinances or statutes of any governmental entities having jurisdiction over the property; underground or above ground storage tanks in area; known remediation sites on property; ongoing mitigation activities or monitoring activities; asbestos; lead-based paint, etc. A phase I environmental study is required for land being acquired in fee by the Public Utility unless waived by Public Utility.

- Physical: inadequate site drainage; proximity to flood zone; erosion issues; wetland overlays; threatened and endangered species; archeological or culturally sensitive areas; inadequate sub-surface elements, etc. Public Utility may require Applicant to procure various studies and surveys as determined necessary by Public Utility.

- Operational: inadequate access for Public Utility's equipment and vehicles; existing structures on land that require removal prior to building of substation; ongoing maintenance for landscaping or extensive landscape requirements; ongoing homeowner's or other requirements or restrictions (e.g., Covenants, Codes and Restrictions, deed restrictions, etc.) on property which are not acceptable to the Public Utility.