## **Inverter Based Resource (IBR) Technical Data Sheet**

Fa	acility Name: Queue # (if known):
	covide a separate data sheet for each type of IBR and each type of transformer Il in data as appropriate according to the type of IBR. Where Not Applicable write NA
1.	Requested Net MW Injection at the POI: MW
	Gross Inverter Nameplate Capability: MVA Station Service Load: MW Mvar
	Additional Information for Storage (For DC-connected batteries, include the following data on the solar inverter data sheet. For AC-connected batteries, complete a separate data sheet.)  MW Rating of Storage: MW for Time: Hours  Gross Energy Rating: MW-HR  Maximum State of Charge: pu  Minimum State of Charge: pu
2.	Simplified One-Line Diagram. This should be similar to the Figure below. If different, mark the differences on the diagram below or provide a new diagram.    Interconnection Transmission
3.	Interconnection Tie Line.
	a) Point of Interconnection (substation or line name):
	b) Line voltage: kV, line rating at 95°F (35°C) ambient: MVA, line length: Miles/Feet
	c) $R_1 = \underline{\hspace{1cm}}$ ohm or $\underline{\hspace{1cm}}$ pu on 100 MVA and line kV base (positive sequence)
	d) $X_1 = \underline{\hspace{1cm}}$ ohm or $\underline{\hspace{1cm}}$ pu on 100 MVA and line kV base (positive sequence)
	e) $B_1 = \underline{\hspace{1cm}} \mu F$ or $\underline{\hspace{1cm}} pu$ on 100 MVA and line kV base (positive sequence)
	f) $R_0 =$ ohm or pu on 100 MVA and line kV base (zero sequence)
	g) $X_0 =$ ohm or pu on 100 MVA and line kV base (zero sequence)

	1) 7
	h) $B_0 = \underline{\hspace{1cm}} \mu F$ or $\underline{\hspace{1cm}} pu$ on 100 MVA and line kV base (zero sequence)
1.	Main Transformer. Number of main transformers:
	Two-Winding Main Transformer Data (as applicable):
	a) Rating (ONAN/ONAF/ONAF):/ MVA
	b) Nominal Voltage for each winding (High/Low): / kV
	c) Winding Connections (High/Low): [Delta or Wye] / [Delta or Wye]
	d) Available tap positions:/// kV or %# of taps.
	e) Positive sequence impedance Z <sub>1</sub> : %, X/R on MVA base.
	f) Zero sequence impedance $Z_0$ : %, X/R on MVA base.
	g) For pad-mounted transformer, construction: 3 / 4 / 5 -legged
	Three-Winding Main Transformer Data (as applicable)
	h) Connection and winding (please attach diagram and mark to reference this form).

	H Winding Data	X Winding Data	Y Winding Data
Full load ratings (i.e. ONAN/ONAF/ONAF)	//	//	//
Rated voltage base	kV Delta or Wye connected	kV Delta or Wye connected	kV Delta or Wye connected
Tap positions available	//kV	//kV	//kV
Present Tap Setting (if applicable)	kV	kV	kV
Neutral solidly grounded? (or) Neutral Grounding Resistor (if applicable)	Ohms	Ohms	Ohms
BIL rating	kV	kV	kV

## Three-Winding Main Transformer Impedance Data (as applicable)

	H-X Winding Data	H-Y Winding Data	X-Y Winding Data	
Transformer base for impedances provided	MVA	MVA	MVA	
Positive sequence impedance Z <sub>1</sub>	% X/R	% X/R	% X/R	
Zero sequence impedance Z <sub>0</sub>	% X/R	% X/R	% X/R	

5.	<b>Collector System Equivalent Model</b> . (Calculated as per "WECC Guide for Representation of Photovoltaic Systems in Large-Scale Load Flow Simulations", January 2011)		
	a)	Collector system one-line diagram attached:	
	b)	Collector system voltage = kV	
	c)	Collector system equivalent impedance:	
		i) $R_1 = \underline{\hspace{1cm}}$ ohm or $\underline{\hspace{1cm}}$ pu on 100 MVA and collector kV base (positive sequence)	
		ii) $X_1 = \underline{\hspace{1cm}}$ ohm or $\underline{\hspace{1cm}}$ pu on 100 MVA and collector kV base (positive sequence)	
		iii) $C_1 = \underline{\hspace{1cm}} \mu F$ or $B_1 = \underline{\hspace{1cm}} pu$ on 100 MVA and collector kV base (positive sequence)	
		iv) $R_0 =$ ohm or pu on 100 MVA and collector kV base (zero sequence)	
		v) $X_0 =$ ohm or pu on 100 MVA and collector kV base (zero sequence)	
		vi) $C_0 = \underline{\hspace{1cm}} \mu F$ or $B_0 = \underline{\hspace{1cm}} pu$ on 100 MVA and collector kV base (zero sequence)	
	d)	Spreadsheet of individual, detailed cable impedances attached:	

6.	Inverter Step-Up Tran	sformers.			
	a) Number of inverter	step-up transformers:	Rating:/	MVA	
	Two-Winding Inverter	· Step-Up Transformer I	Data (as applicable):		
	b) Nominal Voltage fo	r each winding (High/Lov	v): / kV		
	c) Winding Connection	ns: High: Delta or Wye /	Low: Delta or Wye		
	d) Available taps:	///	_/kV or% _	# of taps.	
	e) Positive sequence in	npedance $(Z_1)$ %, _	X/R on MV	/A base.	
	f) Zero sequence impe	dance (Z <sub>0</sub> ) %,	X/R on MVA	base.	
	Three-Winding Invert	er Step-Up Transformer	Data (as applicable)		
	<u> </u>		mark to reference this form	n).	
		H Winding Data	X Winding Data	Y Winding Data	
	ull load ratings .e. ONAN/ONAF/ONAF)	//	//	//	
Rated voltage base		kV Delta or Wye connected	kV Delta or Wye connected	kV Delta or Wye connected	
Tap positions available		//kV	//kV	//kV	
	resent Tap Setting f applicable)	kV	kV	kV	
Neutral solidly grounded? (or) Neutral Grounding Resistor (if applicable)		Ohms	Ohms	Ohms	
BIL rating		kV	kV	kV	
	Three-Winding Inverter Step-Up Transformer Impedance Data (as applicable)				
		H-X Winding Data	H-Y Winding Data	X-Y Winding Data	
Transformer base for impedances provided		MVA	MVA	MVA	
Po	ositive sequence impedance	Z <sub>1</sub>	% % X/R	% X/R	
Zero sequence impedance Z <sub>0</sub>		% X/R		%X/R	

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7	Inverter	and	IRR	Data.

a)	Number of Inverters:
b)	Inverter Capability
	i) at 95°F (35°C): kW/ kVA
	ii) at 113°F (45°C):kW/kVA
c)	Inverter Temperature Derating Curve attached:
d)	Inverter Power Factor: Leading Lagging
e)	IBR kW vs kvar capability curve
	i) at 95°F (35°C) attached:
	ii) at 113°F (45°C) attached:
f)	Inverter Manufacturer and Model #:
g)	IBR Module (e.g. solar panel or battery) Manufacturer and Model #:

h) Provide with this form appropriate verified dynamic models for the IBR. Include a power plant control model that provides volt/var control and active power/frequency control functions, in a Siemens/PTI PSS/E format. Models are expected to represent inverter, plant level controllers and any dynamic reactive resources as they are implemented in the real controls. Power plant controller models must be able to accept external reference values. If multiple IBR types are controlled by a common controller, this functionality must be included in the plant control model. All component models used should be properly integrated with other associated models in the plant model, including any third-party models such that they can send/receive ordered commands as applicable. All models shall be representations of the plant and parameterized to represent known site-specific controls, settings, and protections<sup>1</sup>. Provide BOTH user-written models<sup>2</sup> AND standard library "generic" models<sup>3</sup> (recommended REGCA1, REECA1, REECC1, REECDU1, REPCA1, REPCCU, REPCDU, VTGTPAT and FRQTPAT or similar as requested by Transmission Owner-TO). All the associated files for dynamic modeling should be in PSS/E version 34 and 35 formats.

In addition, the models shall:

<sup>&</sup>lt;sup>1</sup> The default parameters listed in the model software manuals and provided in an initial model package by equipment vendor are typically provided only as a starting point to prevent model initialization issues. Those parameters are not suitable replacements for site-specific parameters. While finalized plant settings are not available during early stages of the interconnection process, the models should be parameterized with control modes and parameters that are as reflective of the intended final design as possible. Model submitters should utilize Duke Energy's IBR interconnection requirements and ensure appropriate parameters are reflected in the model to the best of their ability

<sup>&</sup>lt;sup>2</sup> Also referred to as "user-defined model (UDM)," "user-written model" is used in this document for uniformity. A user-written model is any set of programming code created by equipment manufacturers or developers that captures the latest features of controllers that are mainly software-based and represent the entities' control strategies but does not necessarily correspond to any particular generic library model

<sup>&</sup>lt;sup>3</sup> The term "generic" model is used to describe the industry approved collection of power system component models and are typically available as standard-library models in commercial simulation platforms like PSS/E. Limitations of these models, the model structure, user-selectable options, requirements for scaling the plant size, and representation of protection settings may exist since they are typically not designed specifically for a particular equipment manufacturer

- Include a single DYR file for each model type submission (generic AND user-written) that includes dynamic model records for each control type at a site (inverter, power plant controller, etc.). For battery energy storage sites, separate DYR files could be submitted for charging and discharging modes.
- Include a sample implementation test case. For example: aggregated generator model, aggregated generator transformer, equivalent collector branch, main step-up transformers, tie line, power plant controller, and any other static or dynamic reactive resources. A test case can use a single machine infinite bus representation of the system and must be provided for direct application of "generic" and user-written model file submissions.
- Provide control functions that exhibit appropriate dynamic response compliant with utility requirements including volt/var control, active power/frequency control and ride-through functions.
- Allow the user to determine the allocation of the bus number and machine IDs without restriction.
- Include compiled dynamic linked library (.dll) files for PSS/E version 34 & 35 such that no additional compiling is required for user-written models.
- Include documentation such as user manuals with description of model characteristics, control modes block diagrams, values, description for all model parameters and a list of all state variables.
- Include a user manual to describe procedures and considerations for integrating the model in dynamic simulations, including steady state representation and limitations for model adequacy and usability in the software.

	Check here to indicate all required files are attached:
i)	Provide with this form appropriate Electromagnetic Transient (EMT) models for the IBR, in a Manitoba Hydro PSCAD format. All EMT models are expected be accurate representations of known site-specific controls and protections of the interconnecting facility and comprise of validated equipment EMT models. EMT models must have usability, accuracy, efficiency features in "Duke Energy Electromagnetic Transient Modeling Requirements" checklist found on the respective OASIS sites.
	Check here to indicate all required files are attached:

8.	Pla	ant Reactive Power Compensation (beyond the inverters' built-in reactive capability).
	a)	Type of reactive compensation device(s):
	b)	Individual fixed shunt reactive device type:
		- Number and size of each:× MVA
	c)	Dynamic reactive control device (e.g., SVC, STATCOM):
	d)	Control range: Mvar (lead) to Mvar (lag)
	e)	Control mode (e.g., voltage, power factor, reactive power):
	f)	Regulation point:
	g)	Describe the overall reactive power control strategy:
	h)	Provide with this form the dynamic modeling data in a Siemens/PTI PSS/E standard model. If a user-written model is submitted in place of a generic model, it must include the model characteristics, including block diagrams, values and names for all model parameters, and a list of all state variables. All of the associated files for dynamic modeling should be in the PSS/E version requested by TO and must be shareable on an interconnection-wide basis to support use in the interconnection-wide cases. <sup>4</sup> Check here to indicate all required files are attached:
9.	<b>Sh</b> (a)	ort Circuit Contribution of the Facility at the Point of Interconnection.  Maximum Three Phase Fault Current: Amps and Duration:
	b)	Maximum Single Line to Ground Fault* Current: Amps and Duration:
		del and parameter data required for short-circuit analysis is specific to each PV inverter make and model. All a to be provided in per-unit ohms, on the equivalent inverter MVA base.
		<ul> <li>Inverter Equivalent MVA Base: MVA</li> <li>Short-Circuit Equivalent Pos. Seq. Resistance (R1), valid for initial 4 to 6 cycles: pu.</li> <li>Short-Circuit Equivalent Pos. Seq. Reactance (XL1), valid for initial 4 to 6 cycles: pu.</li> <li>Short-Circuit Equivalent Neg. Seq. Resistance (R2), valid for initial 4 to 6 cycles: pu.</li> <li>Short-Circuit Equivalent Neg. Seq. Reactance (XL2), valid for initial 4 to 6 cycles: pu.</li> <li>Short-Circuit Equivalent Zero Seq. Resistance (R0), valid for initial 4 to 6 cycles: pu.</li> <li>Short-Circuit Equivalent Zero Seq. Reactance (XL0), valid for initial 4 to 6 cycles: pu.</li> <li>Special notes regarding short-circuit modeling assumptions:</li> </ul>
* S	ingle	Line to Ground Fault at the Point of Interconnection with ties to utility at the POI ope

<sup>4</sup> As required by NERC Reliability Standard MOD-32-1.

<sup>7/7 |</sup> P a g e